

EP-A-0 531 713 discloses antifoams based on oil-in-water emulsions whose oil phase contains an alcohol of at least 12 carbon atoms, fatty esters of alcohols of at least 22 carbon atoms and C₁- to C₃₆-carboxylic acids, or fatty esters of C₁₂- to C₂₂-carboxylic acids with monohydric to trihydric C₁- to C₁₈-alcohols or a hydrocarbon having a boiling point above 200°C or fatty acids of 12 to 22 carbon atoms in combination with polyglyceryl esters, which are obtainable by at least 20% esterification of the polyglycerol mixtures with at least one fatty acid of 12 to 36 carbon atoms. These oil-in-water emulsions, too, are stabilized with the aid of a water-soluble emulsifier.

EP-A-0 662 172 discloses antifoams based on oil-in-water emulsions, which are used as antifoams, for example in paper mills, and are still sufficiently effective even at relatively high temperatures of the water circulations. Such antifoams
5 contain, in the oil phase,

- (a) fatty esters of C_{12} - to C_{22} -carboxylic acids with monohydric to trihydric C_1 - to C_{22} -alcohols,
- 10 (b) polyglyceryl esters which are obtainable by at least 20% esterification of polyglycerols which have at least 2 glycerol units with at least one C_{12} - to C_{36} -fatty acid and
- 15 (c) fatty esters of C_{12} - to C_{22} -carboxylic acids and polyalkylene glycols, the molar mass of the polyalkylene glycols being up to 5000 g/mol. The hydrophobic phase can, if required, contain further components, such as alcohols of at least 12 carbon atoms or hydrocarbons having a melting point above 200°C. These oil-in-water emulsions are likewise stabilized
20 with the aid of an emulsifier.

EP-A-0 696 224 discloses aqueous antifoam dispersions whose dispersed phase contains fatty alcohols having melting points above 40°C and ketones having melting points above 45°C and, if
25 required, natural or synthetic waxes having melting points above 50°C.

EP-A-0 732 134 discloses antifoams and/or deaeraters based on oil-in-water emulsions for aqueous media which have a tendency to
30 foam formation, the oil phase of the emulsions containing

- (a) at least one alcohol of at least 12 carbon atoms, distillation residues which are obtainable in the preparation of alcohols having a relatively large number of carbon atoms
35 by oxosynthesis or by the Ziegler process or mixtures of said compounds and
- (b) at least one ester of a sugar alcohol having at least 4 OH groups or at least 2 OH groups and at least one
40 intramolecular ether bond and of a fatty acid of at least 20 carbon atoms in a molar ratio of 1 to at least 1, the free OH groups of this ether being completely or partially esterified, if required, with C_{12} - to C_{18} -carboxylic acids.
- 45 The hydrophobic phase can, if required, contain further antifoam compounds, such as fatty esters of alcohols of at least 22 carbon atoms and C_1 - to C_{36} -carboxylic acids, polyethylene waxes, natural

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The non-prior-published DE-A-19835968.3 discloses antifoams
5 and/or deaeraters which are based on oil-in-water dispersions and
contain, in the hydrophobic oil phase, at least one compound
effective as an antifoam and/or deaerater and, if required,
further components and which are stabilized with the aid of from
0.01 to 3% by weight, based on the oil phase, of a water-soluble,
10 amphiphilic copolymer having acid groups or of a water-soluble
salt thereof. DE-A-19641076 discloses antifoams which are used
both as oil antifoams and in the form of an emulsion antifoam in
the paper industry. The oil phase of the antifoams contains, as
active components, reaction products which are obtainable, for
15 example, by reacting mono- or diglycerides with dicarboxylic
acids and/or their methyl and/or ethyl esters.

It was an object of the present invention to provide novel antifoams and/or deaeraters based on oil-in-water dispersions.

20 We have found that this object is achieved, according to the invention, by antifoams and/or deaeraters based on oil-in-water dispersions which contain, in the dispersed hydrophobic phase, at least one compound effective as an antifoam and/or deaerater and, 25 if required, further components, if the oil phase contains 3-thiaalkan-1-ols, 3-thiaoxoalkan-1-ols, 3-thiadioxoalkan-1-ols, esters of said compounds or mixtures thereof as compounds having an antifoam and/or deaerating effect.

30 The present invention furthermore relates to the use of 3-thiaalkan-1-ols, 3-thiaoxoalkan-1-ols, 3-thiadioxoalkan-1-ols, esters of said compounds or mixtures thereof as components having an antifoam and/or deaerating effect in antifoams and/or deaeraters based on oil-in-water dispersions.

35 3-thiaalkan-1-ols are obtained by reacting α -olefins with mercapto alcohols. The addition of the thiol function of the mercapto alcohols is effected in the presence of oxygen or compounds which, under the reaction conditions (e.g. from 80 to
40 120°C), form free radicals such as peroxides, hydroperoxides or azo compounds, such as azobisisobutyronitrile. The addition reaction of the thioether fatty alcohols with α -olefin takes place by a free radical route with anti-Markovnikov orientation, cf. Angew. Chem. 82 (1970), 276-290, according to the following
45 scheme



10 R is C₈- to C₃₀-alkyl,

R¹ is H, C₁- to C₅-alkyl, preferably CH₃, or phenyl and

R² and R³ are each H, CH₃, C₂H₅ or phenyl.

15 The reaction products, described in the literature, of α -olefins with mercaptoethanol are used, for example, for the preparation of surfactants (cf. US-A-4 040 781) or in hydraulic liquids (cf. US-A-4 031 023). The corresponding 3-thiaoxoalkan-1-ols are

20 obtained from the 3-thiaalkan-1-ols, for example, by oxidation with hydrogen peroxide, PhICl_2 , NaIO_4 , tert-BuOCl , potassium permanganate, tungstic acids or per acids (e.g. peracetic acid or perbenzoic acid).

25 3-Thiadioxoalkan-1-ols are likewise obtainable from the
3-thiaalkan-1-ols by oxidation with said oxidizing agents, except
that different reaction conditions are employed, for example the
concentration of the oxidizing agent and the temperature at which
the oxidation is carried out are increased.

30 The corresponding esters are obtained from the 3-thiaalkan-1-ols, the 3-thiaoxoalkan-1-ols and the 3-thiadioxoalkan-1-ols by esterification with acids. For example, it is possible to prepare esters of phosphoric acid, sulfuric acid or carbonic acid as well
35 as esters of organic acids, for example esters of the thia compounds with C₁- to C₃₀-carboxylic acids, phosphonic acids or sulfonic acids. In addition to monocarboxylic acids, di- and polycarboxylic acids, such as adipic acid, tartaric acid and citric acid, are also suitable. Particularly preferred components
40 for the novel antifoams are C₁₆- to C₂₄-carboxylic acids, such as palmitic acid, oleic acid, stearic acid and behenic acid.

3-Thiaalkan-1-ols, 3-thiaoxoalkan-1-ols, 3-thiadioxoalkan-1-ols, esters of said compounds or mixtures thereof, either alone or in
45 combination with known compounds effective as antifoams and/or deaeraters, can form the hydrophobic phase of antifoams and/or

deaeraters. The hydrophobic phase of novel antifoams and/or deaeraters may contain, for example, the following components:

- (a) 3-thiaalkan-1-ols, 3-thiaoxoalkan-1-ols,
 3-thiadioxoalkan-1-ols, esters of said compounds or mixtures thereof and
- (b) at least one compound from the group consisting of the glyceryl esters of fatty acids having at least 10 carbon atoms in the molecule, C₁₂- to C₃₀-alcohols, alkoxyated alcohols, esters of sugar alcohols having at least 4 OH groups or at least 2 OH groups and at least one intramolecular ether bond and of a fatty acid having at least 20 carbon atoms in the molecule, fatty esters of C₁₂- to C₂₂-carboxylic acids with monohydric to trihydric alcohols, ketones having melting points above 45°C, the polyglyceryl esters which are obtainable by at least 20% esterification of polyglycerols which have at least 2 glycerol units with at least one C₁₂- to C₃₆-fatty acid, reaction products of mono- and diglycerides with dicarboxylic acids, reaction products of glycerol with dicarboxylic acids, which reaction products are esterified with at least one C₁₂- to C₃₆-fatty acid, polyethylene waxes, natural waxes, hydrocarbons having boiling points above 200°C, finely divided inert solids and mixtures of said compounds.

Preferred antifoams and/or deaeraters are those whose oil phase contains

- (a) 3-thiaalkan-1-ols, 3-thiaoxoalkan-1-ols,
 3-thiadioxoalkan-1-ols, carboxylic esters of said compounds or mixtures thereof,
- (b1) polyglyceryl esters which are obtainable by at least 20% esterification of polyglycerols which have at least 2 glycerol units with at least one C₁₂- to C₃₆-fatty acid and
- (b2) glyceryl esters of fatty acids having at least 10 carbon atoms in the molecule, C₁₂- to C₃₀-alcohols, alkoxyated alcohols, esters of sugar alcohols having at least 4 OH groups or at least 2 OH groups and at least one intramolecular ether bond and of a fatty acid having at least 20 carbon atoms in the molecule, fatty esters of C₁₂- to C₂₂-carboxylic acids with monohydric to trihydric alcohols, ketones having melting points above 45°C, reaction products of mono- and diglycerides with dicarboxylic acids, reaction products of glycerol with dicarboxylic acids, which reaction

The hydrophobic phase of the antifoams and/or deaeraters contains, as component (a), for example, from 1 to 100% by weight of a 3-thiaalkan-1-ol, of a 3-thiaoxoalkan-1-ol, of a 3-thiadioxoalkan-1-ol, of an ester of said compounds or of

10 mixtures thereof. The hydrophobic phase of the antifoams and/or
deaeraters preferably contains from 5 to 75% by weight of a
3-thia-C₁₆- to C₃₀-alkan-1-ol, of a 3-thiaoxo-C₁₆- to
C₃₀-alkan-1-ol, of a 3-thiadioxo-C₁₆- to C₃₀-alkan-1-ol or of
mixtures thereof. Particularly preferred antifoams and/or
15 deaeraters are those whose hydrophobic phase contains from 5 to
85% by weight of a 3-thia-C₁₈- to C₂₈-alkan-1-ol. The compounds of
component (b) account for from 25 to 95, preferably from 30 to
95, % by weight of the oil phase. In the case of the preferred
antifoams, the amount of component (b1) is from 2 to 20% by
20 weight and that of component (b2) is from 13 to 75% by weight.

The component (b) of the antifoams and/or deaeraters comprises all compounds which are known as antifoams and/or deaeraters.

Examples of these are glyceryl esters of fatty acids having at least 10 carbon atoms in the molecule. Further suitable compounds are C₁₂- to C₃₀-alcohols, such as myristyl alcohol, cetyl alcohol, stearyl alcohol, palmityl alcohol, tallow fatty alcohol and behenyl alcohol, and synthetic alcohols, for example saturated, straight-chain, unbranched alcohols obtainable by oxidation of

30 alkylaluminums by the Ziegler process. Synthetic alcohols are also obtained by oxosynthesis. These are as a rule alcohol mixtures. The alcohols may contain, for example, up to 48 carbon atoms in the molecule. Very effective antifoams contain, for example, mixtures of at least one C₁₂- to C₂₆-alcohol and at least
35 one fatty alcohol having 28 to 48 carbon atoms in the molecule, cf. EP-A-0 322 830. Instead of the pure alcohols, distillation residues which are obtainable in the preparation of alcohols having a relatively large number of carbon atoms by oxosynthesis or by the Ziegler process can also be used as antifoam compounds.

40 Further compounds which are suitable as antifoams and/or deaerators are alkoxyated alcohols and alkoxyated distillation residues which are obtained in the preparation of alcohols by oxosynthesis or by the Ziegler process. The alkoxyated compounds are obtainable by reacting the long-chain alcohols or

45 distillation residues with ethylene oxide or with propylene oxide
or with a mixture of ethylene oxide and propylene oxide. It is
possible to subject first ethylene oxide and then propylene oxide

5 the group consisting of the alkoxyated compounds are those reaction products which are prepared by subjecting one or two moles of ethylene oxide to an addition reaction with one mole of fatty alcohol or distillation residue.

- 10 The abovementioned fatty alcohols having at least 12 carbon atoms in the molecule are generally used together with other compounds likewise acting as antifoams. Such compounds are, for example, fatty esters of C₁₂- to C₂₂-carboxylic acids with monohydric to trihydric C₁-C₁₈-alcohols. The fatty acids on which these esters
15 are based are, for example, lauric acid, myristic acid, palmitic acid, stearic acid, arachidic acid and behenic acid. Palmitic acid or stearic acid is preferably used. Monohydric C₁- to C₁₈-alcohols can be used for esterifying said carboxylic acids, e.g. methanol, ethanol, propanol, butanol, hexanol, dodecanol and
20 stearyl alcohol, or dihydric alcohols such as ethylene glycol, or trihydric alcohols, e.g. glycerol. The polyhydric alcohols may be completely or only partially esterified.

Further compounds having an antifoam and deaerating effect are

- 25 polyglyceryl esters. Such esters are prepared, for example, by esterifying polyglycerols which contain at least 2 glycerol units with at least one C₁₂- to C₃₆-carboxylic acid. The polyglycerols on which the esters are based are esterified to such an extent that compounds which are virtually insoluble in water form. The
30 polyglycerols are obtained, for example, by condensation of glycerol under alkaline catalysis at relatively high temperatures or by reacting epichlorohydrin with glycerol in the presence of acidic catalysts. The polyglycerols usually contain from at least 2 to about 30, preferably from 2 to 12, glycerol units.
- 35 Commercial polyglycerols contain mixtures of polymeric glycerols, for example mixtures of diglycerol, triglycerol, tetraglycerol, pentaglycerol and hexaglycerol and possibly polyglycerols having a higher degree of concentration. The degree of esterification of the OH groups of the polyglycerols is from at least 20 to 100,
40 preferably from 60 to 100, %. The long-chain fatty acids used for the esterification may be saturated or ethylenically unsaturated. Suitable fatty acids are, for example, lauric acid, myristic acid, palmitic acid, stearic acid, arachidic acid, behenic acid, oleic acid, hexadecanoic acids, elaidic acid, eicosenoic acids,
45 docosenoic acids, such as erucic acid, or polyunsaturated acids, such as octadecadienoic acids and octadecatrienoic acids, e.g. linoleic acid and linolenic acid, and mixtures of said carboxylic

acids. Polyglyceryl esters suitable as antifoams are described, for example, in EP-A-0 662 172.

- Other compounds which are suitable as antifoams and/or deaeraters
- 5 for aqueous media having a tendency to foam formation and which are used either alone or together with at least one alcohol of at least 12 carbon atoms are esters of a sugar alcohol having at least 4 OH groups or at least 2 OH groups and at least one intramolecular ether bond and of a fatty acid having at least 20
 - 10 carbon atoms in the molecule in a molar ratio of 1 to at least 1, where the free OH groups of these esters may be partially or completely esterified with C₁₂- to C₁₈-carboxylic acids. Esters of tetritols, pentitols and/or hexitols with fatty acids of at least 22 carbon atoms in a molar ratio of 1 to at least 1.9 are
 - 15 preferably used. Esters of mannitol and/or sorbitol with behenic acid in a molar ratio of 1 to at least 1, preferably 1 to at least 1.9, are particularly preferably employed. In addition to the suitable sugar alcohols sorbitol and mannitol, adonitol, arabitol, xylitol, dulcitol, pentaerythritol, sorbitan and
 - 20 erythritol are useful. Sugar alcohols are understood as meaning the polyhydroxy compounds which are formed from monosaccharides by reduction of the carbonyl function and are not themselves sugars. The anhydro compounds which form from sugar alcohols by intramolecular water elimination may also be used. Particularly
 - 25 effective antifoams and/or deaeraters are obtained if sugar alcohols are esterified with C₂₂- to C₃₀-fatty acids. If the sugar alcohols are only partially esterified with a fatty acid of at least 20 carbon atoms, the unesterified OH groups of the sugar alcohol can be esterified with another carboxylic acid, for
 - 30 example a C₁₂- to C₁₈-carboxylic acid can be used. Esters of this type are described in EP A-0 732 134.

- Further compounds suitable as antifoams and/or deaeraters are ketones having melting points above 45°C. They are generally used
- 35 together with fatty alcohols whose melting points are above 40°C. Such antifoam mixtures are known from EP A-0 696 224, mentioned in connection with the prior art. The reaction products, disclosed in DE-A 196 41 076, of, for example, mono- and/or diglycerides with dicarboxylic acids and reaction products of
 - 40 glycerol with dicarboxylic acids, which reaction products have been esterified with at least one C₁₂- to C₃₆-fatty acid, are also suitable as additives to the hydrophobic phase of the novel antifoams and/or deaeraters.
 - 45 Other compounds which enhance the efficiency of long-chain alcohols as antifoams and are therefore also used in antifoam mixtures are, for example, polyethylene waxes having a molar mass

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of at least 2000 and natural waxes, such as bees' wax or carnauba wax.

A further component of antifoam mixtures comprises hydrocarbons having a boiling point above 200°C (determined at atmospheric pressure). Preferably used hydrocarbons are liquid paraffins, for example the commercially available paraffin mixtures which are also referred to as white oil. Paraffins whose melting point is, for example, above 50°C are also suitable.

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The abovementioned compounds which are effective as antifoams and/or deaeraters are used either alone or as a mixture with one another for the preparation of antifoam and deaerater dispersions. They can be mixed with one another in any desired ratio. The mixing of the compounds and also the emulsification in water are effected at relatively high temperatures. The effective components which form the oil phase of the antifoam mixture are, for example, heated to above 40°C, for example from 70 to 120°C, and are emulsified in water under the action of shearing forces so that oil-in-water emulsions are obtained. Commercial apparatuses are used for this purpose. The particle size of the dispersed hydrophobic phase is, for example, generally from 0.4 to 15 µm and from 0.2 to 40 µm, preferably from 0.5 to 5 µm. The finely divided oil-in-water emulsions thus obtained are stabilized, for example, with water-soluble, amphiphilic copolymers having acid groups or with water-soluble salts thereof. The procedure which may be used here is, for example, to add from 0.01 to 3% by weight, based on the total emulsion, of a water-soluble amphiphilic copolymer having acid groups or of a water-soluble salt thereof to the oil-in-water emulsion directly after the homogenization or to emulsify the compounds acting as antifoams and/or deaeraters in an aqueous solution of a water-soluble, amphiphilic copolymer having acid groups or of a salt thereof. Dispersions having a long shelf life are obtained in this manner after cooling to room temperature. The organic phase dispersed in water accounts for, for example, from 5 to 50, preferably from 10 to 35, % by weight of the oil-in-water dispersions.

40 After cooling to room temperature, the oil phase dispersed in water becomes solid so that dispersions which have a long shelf life are obtained.

The novel oil-in-water dispersions can, if required, contain
45 finely divided, virtually water-insoluble, inert solids having
particle sizes of $<20\text{ }\mu\text{m}$, preferably from 0.1 to $10\text{ }\mu\text{m}$, in an
amount of, for example, from 0.1 to 50 , preferably from 1 to 35 ,

Antifoam dispersions which contain from 0.01 of 3% by weight of a water-soluble, amphiphilic copolymer having acid groups or of a salt thereof are particularly advantageous.

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- 30

The invention also relates to the use of

- 40 - polymers of monoethylenically unsaturated acids having molar masses of from 1500 to 300,000,
- graft polymers of from 5 to 40 parts by weight of
- 45 n-vinylformamide per 100 parts by weight of a polyalkylene glycol having a molar mass of from 500 to 10,000,

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The amphiphilic copolymers contain units of

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(a) from 45 to 80% by weight of styrene,

(b) from 55 to 20% by weight of acrylic acid and, if required,

(c) additionally further monomers

10 as polymerized units. The copolymers can, if required, contain units of monoesters of maleic acid as polymerized further monomers (c). Such copolymers are obtainable, for example, by copolymerizing copolymers of styrene, diisobutene or isobutene or mixtures thereof with maleic anhydride in the absence of water

15 and reacting the copolymers with alcohols after the polymerization, from 5 to 50 mol% of a monohydric alcohol being used per mole of anhydride groups in the copolymer. Suitable alcohols are, for example, methanol, ethanol, n-propanol, isopropanol, n-butanol, isobutanol and tert-butanol. However, it

20 is also possible to react the anhydride groups of the copolymers with polyhydric alcohols, such as glycol or glycerol. Here, however, the reaction is continued only until only one OH group of the polyhydric alcohol reacts with the anhydride group. If the anhydride groups of the copolymers are not all reacted with

25 alcohols, the anhydride groups not reacted with alcohols undergo ring opening as a result of the addition of water.

Other compounds to be used as a stabilizer are, for example, commercial polymers of monoethylenically unsaturated acids and

30 graft polymers of N-vinylformamide on polyalkylene glycols, which are described, for example, in WO-A-96/34903. If required, up to 10% of the vinylformamide units grafted on may be hydrolyzed. The amount of vinylformamide units grafted on is preferably from 20 to 40% by weight, based on polyalkylene glycol. Preferably, 35 polyethylene glycols having molar masses of from 2000 to 10,000 are used.

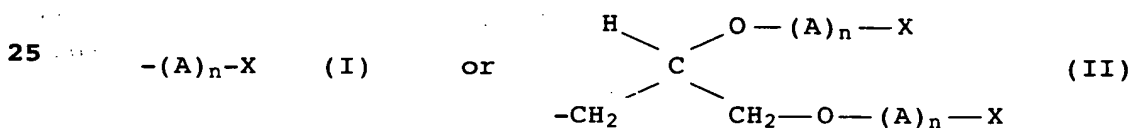
The zwitterionic polyalkylenepolyamines and zwitterionic polyethyleneimines also suitable as stabilizers are disclosed.

40 for example, in EP-B-0112592. Such compounds are obtainable, for example, by first alkoxyating a polyalkylene polyamine or polyethyleneimine, for example with ethylene oxide, propylene oxide and/or butylene oxide, and then quaternizing the alkoxylation products, for example with methyl bromide or

45 dimethyl sulfate, and then sulfating the quaternized, alkoxyated products with chlorosulfonic acid or sulfur trioxide. The molar mass of the zwitterionic polyalkylenepolyamines is, for example,

from 1000 to 9000, preferably from 1500 to 7500. The zwitterionic polyethyleneimines preferably have molar masses of from 2000 to 1700 dalton.

- 5 Zwitterionic polyetherpolyamines suitable as stabilizers are obtainable, for example, by reacting, in a first reaction stage, linear or branched polyetherpolyamines having molar masses of from 100 to 800 and containing 2 to 10 nitrogen atoms and at least two primary or secondary terminal amino groups or the
- 10 reaction products of said polyetherpolyamines with up to one mole of glycidol per NH group of the polyetherpolyamines with at least one C₂- to C₄-alkylene oxide or tetrahydrofuran in an amount such that from 1 to 50 alkylene oxide units undergo addition per NH group in the polyetherpolyamines. In a second process step, the
- 15 alkoxylated polyetherpolyamines are reacted with a compound selected from the group consisting of halosulfonic acids, halophosphoric acids, vinylsulfonic acid, propanesultone, haloacetic acids, acrylic acid, methacrylic acid, vinylphosphoric acid and the alkali metal or ammonium salts of said acids in a
- 20 manner such that at least one terminal tertiary amino group of the alkoxylated polyetherpolyamines contains 2 groups of the formula



where

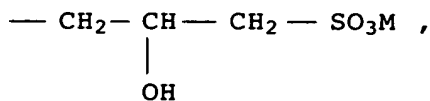
- 30 A is an ethylene oxide, propylene oxide, butylene oxide or tetrahydrofuran unit,

n is from 1 to 50,

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X is $-\text{SO}_3\text{M}$, $-\text{CH}_2-\text{CH}_2-\text{SO}_3\text{M}$, $-\text{CH}_2-\text{CH}_2-\text{CH}_2-\text{SO}_3\text{M}$,

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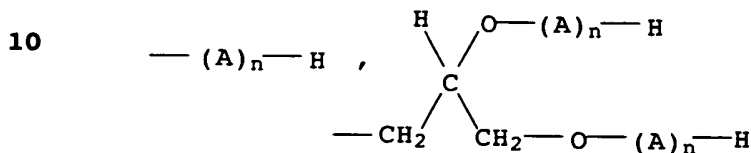
$-\text{CH}_2-\text{COOM}$, $-\text{CH}_2-\text{CH}_2-\text{COOM}$,

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$-\text{PO}_3\text{M}_2$, $-\text{CH}_2-\text{CH}_2-\text{PO}_3\text{M}_2$,

it being possible, in the formula II, for one substituent X also to be hydrogen, and

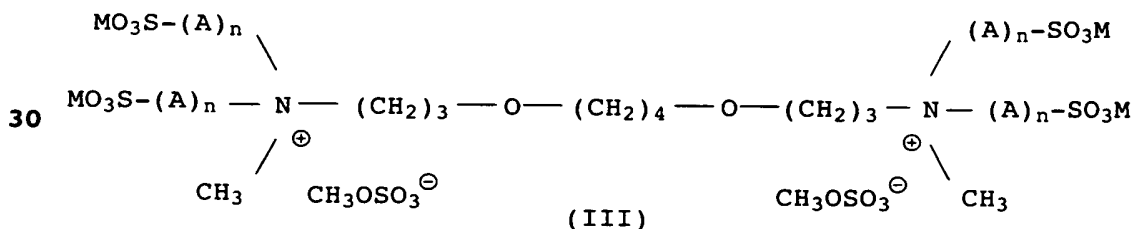
M is hydrogen, an alkali metal or ammonium. At least one terminal
5 tertiary amino group of the alkoxyated polyetherpolyamine can however also contain only one group of the formula I or II and one group of the following structures



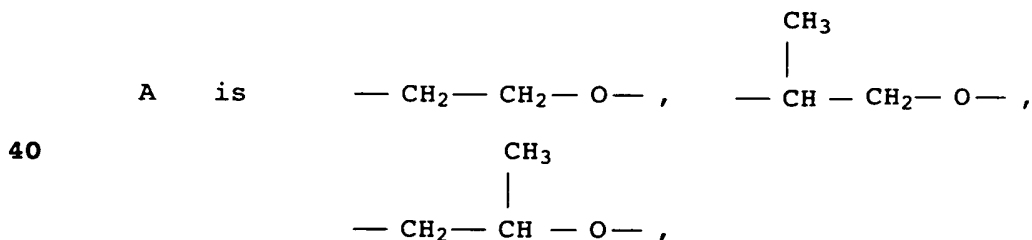
15 C₁- to C₂₂-alkyl or C₇- to C₂₂-aralkyl, where A and n have the same meanings as in the formulae I and II.

In a 3rd process stage, the reaction product obtained in the 2nd
process stage is quarternized. The quarternization can however
20 also be achieved by quaternizing the product obtainable in the 1st reaction stage and then carrying out the reaction stated in the 2nd reaction stage.

Of particular industrial interest as stabilizers are zwitterionic
25 polyetherpolyamines of the formulae

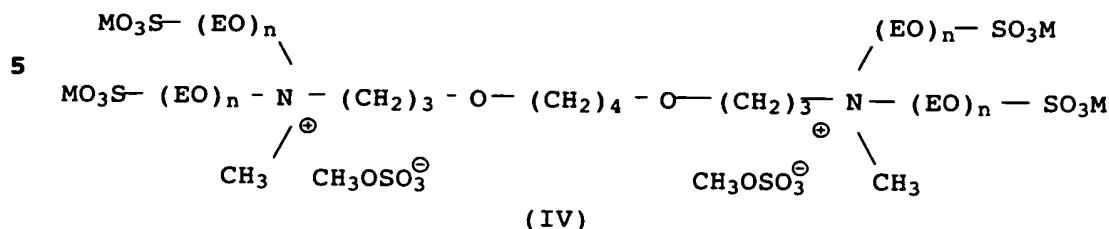


35 where



45 M is H, Na, K or ammonium and
n is 15-25,

and



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where

EO is $-\text{CH}_2-\text{CH}_2-\text{O}-$

M is H, Na, K or ammonium and

15 n is 15-25.

The molar mass of the zwitterionic polyetherpolyamines is, for example, up to 9000, preferably from 1500 to 7500.

- 20 Zwitterionic crosslinked polyamines which are also suitable as a stabilizer for oil-in-water dispersions are obtainable, for example, by reacting aliphatic or araliphatic monoamines or polyamines having from 2 to 5 primary, secondary or tertiary nitrogen groups with a crosslinking agent, for example in a ratio
- 25 of from 20:1 to 1:1, based on molar amounts of amino groups in the amines and molar amounts of reactive groups in the crosslinking agents, with formation of crosslinked polyamines having molar masses of from 150 to 1500, alkoxylating the crosslinked amines, then introducing an anionic group into the
- 30 resulting product by reacting these compounds, for example with a halosulfonic acid, halophosphoric acid, vinylsulfonic acid, propanesulfonic acid, haloacetic acid, acrylic acid, methacrylic acid, vinylphosphoric acid or the alkali metal or ammonium salts of said compounds containing acid groups, and then quarternizing
- 35 the products, for example with methyl bromide and dimethyl sulfate, it being possible to effect the quaternization also directly after the alkoxylation of the crosslinked polyamines. Furthermore, the polyetheramines described above may be used as polyamines. For example, suitable stabilizers can be prepared by
- 40 reacting 4,9-dioxadodecane-1,12-diamine with epichlorohydrin in a molar ratio of 2:1, ethoxylating the reaction product obtainable, for example 20 mol of ethylene oxide undergoing addition per NH group, then quarternizing the reaction product with dimethyl sulfate and sulfating the quarternized product in a further
- 45 reaction stage by reaction with SO_3 or chlorosulfonic acid.

Suitable stabilizers for the novel antifoams and/or deaerators are preferably homopolymers of acrylic acid, homopolymers of methacrylic acid, copolymers of acrylic acid and methacrylic acid in any desired molar ratio, copolymers of acrylic acid and maleic acid in any desired molar ratio, copolymers of methacrylic acid and maleic acid, polyvinylsulfonic acid, polyacrylamido-2-methylpropanesulfonic acid, styrenesulfonic acid and the alkali metal and ammonium salts of said polymers having molar masses of, for example, from 1500 to 300,000.

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The novel antifoams and/or deaerators are very effective in aqueous systems which tend to foam, both at room temperature and at higher temperatures, for example at above 40°C. They have substantially improved long-term effect compared with known

- antifoams. The aqueous dispersions are preferably used as antifoams and/or deaerators for foam control of aqueous media having to tendency to foam formation, for example in the food industry, in the starch industry and in wastewater treatment plants. Of particular interest, however, is the use of the antifoams and/or deaerators for foam control in pulp cooking, in pulp washing, in the beating of paper stock, in paper making and in the dispersing of pigments for paper making. In these processes, the temperature of the aqueous medium to be defoamed is generally above 40°C, for example from 45 to 75°C. The novel mixtures based on oil-in-water dispersions act both as antifoams and as deaerators. In some cases, the deaerating effect is more pronounced than the antifoam effect. They can be used as antifoams or deaerators. They are also advantageously used in the engine sizing and surface sizing of paper. When these mixtures are used in paper stock suspensions, for example, their deaerating effect is to the forefront. For example, up to 0.5, preferably from 0.002 to 0.3, % by weight of the deaerater are used per 100 parts by weight of paper stock in a foam-forming medium.

35

In the examples which follow, parts and percentages are by weight, unless stated otherwise in the examples.

Examples

40

- The tendency of the dispersions to cream was determined using the centrifuge test. For this purpose, the dispersion was poured into a 97 mm long centrifuge tube to a height of 75 mm and centrifuged for 30 minutes at 5000 rpm. The larger the amount of water which had separated off at the bottom, the lower the stability of the

dispersion. The height from the bottom of the centrifuge tube to the front of the oil phase was measured.

The deaerating effect was determined with the aid of a Sonica measuring instrument, the antifoam being added to a 0.38% strength paper stock suspension at 40°C exactly in an amount which gave a concentration of 5 ppm, based on the oil phase (active substance), of antifoam. The air content was determined continuously by means of ultrasound attenuation before the metering of the antifoams and during the first 5 minutes after metering. The air content initially decreased and increased again toward the end of the measurement. In each case, the minimum air content of the paper stock suspension in % by volume is stated in the table. This method of measurement is described in TAPPI Journal 71 (1988), 65-69.

Said paper stock suspension was used in all examples and comparative examples. Before the addition of a deaerater, it contained 1.44% by volume of air. In the table, the air content in % by volume after metering of the deaeraters is stated under the header minimum air content. The smaller this number, the more effective is the deaerater.

The long-term effect of the antifoams or deaeraters was determined by comparing the air content of the paper stock suspension after 5 minutes with the minimum air content (immediately after the metering of the deaerater). The value shown in the table for the long-term effect is the difference between the value for the deaerating effect after 5 minutes and the value which is measured immediately after the metering. The smaller the value, the better the long-term effect.

The antifoam activity was determined in a foam channel, likewise at 50°C, a paper stock suspension which was foamed by introduction of air being added to the antifoam. The foam protuberance was formed two-dimensionally on the vertical wall of the foam channel and counted in cm². This method is disclosed in the literature, cf. F. Poschmann, Das Papier 15, 295-301 (1961).

The stated particle sizes are mean values which were determined with the aid of a Coulter LS 230 apparatus using about 0.1% strength dispersions. The apparatus operates according to the principle of Fraunhofer diffraction.

Preparation of 3-thiaalkan-1-ols

Thiaalkanol A

In a V2A stainless steel reactor, 402 g (1.3 mol) of a
 5 C₂₀-/C₂₄- α -olefin mixture (melting point about 50°C) were heated to
 65°C. Thereafter, 101.5 g (1.3 mol) of 2-mercaptoethanol were
 added dropwise in the course of 30 minutes and an air stream was
 passed continuously over the reaction mixture. The temperature of
 the reaction mixture increased to 84°C during the addition of the
 10 mercaptoethanol. After the end of the addition of
 mercaptoethanol, the reaction mixture was stirred for a further
 10 hours at 100°C and unreacted mercaptoethanol was then distilled
 off. Residual volatile impurities were then removed with the aid
 of steam distillation. 398 g of a colorless wax having a melting
 15 point of about 65°C were obtained.

Thiaalkanol B

In a V2A stainless steel reactor equipped with a stirrer, 309 g
 (1.0 mol) of a C₂₀-/C₂₄- α -olefin mixture having a melting point of
 20 about 50°C were heated to 80°C. 70 g (0.9 mol) of
 2-mercaptoethanol were added dropwise to the melt in the course
 of 30 minutes and at the same time an air stream was passed over
 the reaction mixture. The temperature increased to 84°C. After
 addition of the mercaptoethanol, the reaction mixture was stirred
 25 for a further 20 hours at 90°C until the mercaptoethanol content
 was below 0.3%. Thereafter, the reaction mixture was cooled to
 75°C and the volatile fractions were then removed at 75 mbar. 378
 g of a colorless wax having a melting point of about 65°C were
 obtained.

30

Thiaalkanol C

309 g (1.0 mol) of a C_{20/24} α -olefin mixture (melting point about
 50°C) and 70 g (0.9 mol) of mercaptoethanol were metered
 35 simultaneously into a V2A stainless steel reactor over a period
 of 30 minutes and at the same time an air stream was passed over
 the reaction mixture. The temperature increased to 95°C. After
 metering was complete, stirring was carried out for 20 hours at
 90°C until the mercaptoethanol content had fallen below 0.3% by
 40 weight. Thereafter, the reaction mixture was cooled to 75°C and

the volatile fractions were then removed at 75 mbar. 365 g of a colorless wax having a melting point of about 65°C were obtained.

Thiaalkanol D

5

The procedure was as described in the preparation of thiaalkanol B, except that in this case 0.8 mol of 2-mercaptoethanol was used instead of 0.9 mol of 2-mercaptoethanol.

10 Thiaalkanol E

Preparation as described for thiaalkanol B but with the only exception that 0.95 mol of 2-mercaptoethanol was used.

15 Thiaalkanol F

Preparation as for thiaalkanol B, except that 0.85 mol of 2-mercaptoethanol was used.

20 Example 1

An oil-in-water emulsion in which the oil phase accounted for 27.3% by weight of the dispersion and had a mean particle size of from 0.9 to 10 μm was prepared with the aid of an Ultraturrax and
25 of a high-pressure homogenizer from APV Gaulin GmbH.

The hydrophobic phase consisted of the following components:

- (a) 664 parts of the thiaalkanol B,
30
- (b) 56 parts of a polyglyceryl ester which is obtainable by esterifying a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with
35 behenic acid (degree of esterification 100%) and

- (c) 254.8 parts of glyceryl triesters of C_{16} - to C_{18} -fatty acids.

The aqueous phase consisted of:

40

- 2560 parts of demineralized water,
- 28 parts of a 40% strength aqueous, ammoniacal solution of an amphiphilic copolymer of 50 parts of acrylic acid and 50 parts of styrene, having an acid number of 320 mg of KOH/g of polymer and
45 a molar mass of 5500 and 3.5 parts of a xanthan gum.

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The aqueous solution was heated to 95°C.

The abovementioned components (a) to (c) were first heated to 90°C and then emulsified in the aqueous phase heated to 95°C, with
 5 great shearing with an Ultraturrax for 2 minutes. The emulsion was divided into 3 parts which were then emulsified at 10, 20 and 40 bar by means of a high-pressure homogenizer and in each case cooled to room temperature in an ice bath immediately after the emulsification. The properties of the dispersions thus obtained
 10 are shown in Table 1.

Example 2

As described in Example 1, an oil-in-water dispersion was
 15 prepared in which the hydrophobic phase consisted of the following components:

- (a) 92 parts of the thiaalkanol A,
- 20 (b) 8 parts of a polyglyceryl ester which is obtainable by esterifying a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with a C₁₂- to C₂₆-fatty acid mixture (degree of esterification
 25 60%) and
- (c) 36.4 parts of glyceryl triesters of C₁₈-fatty acids.

The aqueous phase consisted of 360 parts of water, 5 parts of a
 30 27% strength aqueous, ammoniacal solution of an amphiphilic copolymer of 25 parts of acrylic acid and 75 parts of styrene, having a molar mass of 16,000 D and an acid number of 240 mg of KOH/g of polymer.

35 The components (a) to (c) were mixed, first heated to 110°C, then introduced with great shearing by means of an Ultraturrax in the course of 15 seconds into an aqueous solution heated to 80°C, then emulsified for 45 seconds and, immediately after the emulsification, cooled to room temperature by means of an ice
 40 bath. The properties of the dispersion are shown in Table 1.

Example 3

According to Example 1, an oil-in-water dispersion was prepared
 45 in which the hydrophobic phase consisted of

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(a) 92 parts of the thiaalkanol D,

(b) 8 parts of a polyglyceryl ester which was prepared by esterifying a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with behenic acid (degree of esterification 100%) and

(c) 36.4 parts of glyceryl triesters of C₁₆- to C₁₈-fatty acids.

10

The aqueous phase consisted of 360 parts of demineralized water, 4 parts of a 40% strength ammoniacal solution of an amphiphilic copolymer of 50 parts of acrylic acid and 50 parts of styrene (molar mass 5500, acid number 320 mg of KOH/g of polymer) and 0.5

15 part of a xanthan gum. The abovementioned components (a) to (c) were first heated to 90°C, then introduced with great shearing by means of an Ultraturrax in the course of 15 seconds into the aqueous phase heated to 95°C, then emulsified for 45 seconds and, immediately after the emulsification, cooled to room temperature

20 in an ice bath. The properties of the dispersion are shown in Table 1.

Example 4

25 With the aid of an Ultraturrax, an oil-in-water dispersion was prepared in which the oil phase accounted for 27.3% of the dispersion and had a mean particle size of from 0.9 to 10 µm. The hydrophobic phase consisted of the following components:

30 (a) 92 parts of the thiaalkanol E,

(b) 8 parts of a polyglyceryl ester which was prepared by esterifying a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with behenic acid (degree of esterification 100%) and

(c) 36.4 parts of glyceryl esters of C₁₆- to C₁₈-fatty acids.

40 The aqueous phase consisted of 360 parts of demineralized water, 4 parts of a 40% strength aqueous ammoniacal solution of an amphiphilic copolymer of 50 parts of acrylic acid and 50 parts of styrene (molar mass 5500, acid number 320 mg of KOH/g of polymer) and 0.5 part of a commercial xanthan gum. The components (a) to

45 (c) of the hydrophobic phase were mixed, heated to 90°C, then introduced with great shearing by means of an Ultraturrax in the course of 15 seconds into the aqueous phase heated to 95°C, and

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According to Example 1, an oil-in-water dispersion was prepared by emulsifying an oil phase comprising

- 30 Comparative example

35 (a) 18 parts of a glyceryl triester of C₁₆- to C₁₈-fatty acids,

(b) 5 parts of a polyglyceryl ester which was prepared by esterifying a polyglycerol mixture comprising 27% of

40 diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with a C₁₂- to C₂₆-fatty acid mixture (degree of esterification 60%) and

45

- (c) 2 parts of a fatty ester which is obtainable by esterifying a C_{16} - to C_{18} -fatty acid mixture with a block copolymer comprising ethylene oxide and propylene oxide in a molar ratio of 3 : 7, having a molecular weight of 1200 g/mol.

5

The components (a) to (c) were mixed, first heated to 110°C and then emulsified in an aqueous phase comprising 70 parts of demineralized water, 3 parts of an emulsifier which is obtainable by subjecting 25 mol of ethylene oxide to an addition reaction
10 with 1 mol of isooctylphenol and esterifying the adduct with sulfuric acid to give the monoester, and 1 part of a copolymer of 70% of acrylamide and 30% of acrylic acid, having a K value of 270, and 0.2 part of sodium hydroxide solution. For this purpose, the aqueous phase was first heated to 80°C and the hydrophobic
15 phase was emulsified with great shearing by means of an Ultraturrax in the course of one minute. Immediately after the emulsification, the mixture was cooled to room temperature in an ice bath. The properties of the dispersion thus obtained are shown in Table 1.

20

Example 6

According to Example 1, an oil-in-water dispersion was prepared in which the oil phase had the following composition:

25

- (a) 644 parts of thiaalkanol C,

- (b) 56 parts of a polyglyceryl ester which is obtainable by esterifying a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10%
30 of polyglycerols having a higher degree of condensation with behenic acid (degree of esterification 100%) and

- (c) 254.8 parts of glyceryl triesters of C_{16} - C_{18} -fatty acids.

35

The aqueous phase consisted of:

- 2560 parts of demineralized water,
12 parts of a polyglyceryl ester of polyglycerol having an
40 average molar mass of 200 and oleic acid in a molar ratio of 1 : 1.7 and
3.5 parts of a xanthan gum.

- The aqueous solution was processed with components (a), (b) and
45 (c) as described in Example 1 at 20 and 40 bar to give an oil-in-water dispersion.

Example 7

An oil-in-water dispersion was prepared by initially taking a hydrophobic phase comprising

- 5
- (a) 92 parts of the thiaalkanol B,
- (b) 8 parts of a polyglyceryl ester which is obtainable by esterifying a polyglycerol mixture comprising 27% of
- 10 diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with behenic acid (degree of esterification 100%),
- (c) 16 parts of a hydrogenated castor oil having an iodine number
- 15 of < 5 and
- (d) 4 parts of a finely divided kaolin in which 98% of the particles had a size of < 2 μm
- 20 with vigorous stirring by means of an Ultraturrax at 85°C and introducing the heated aqueous phase consisting of
- 370 parts of demineralized water and
- 2.5 parts of a 40% strength aqueous ammoniacal solution of an
- 25 amphiphilic copolymer of 50 parts of acrylic acid and 50 parts of styrene (molar mass 5500, acid number 320 mg of KOH/g of polymer) in the course of 20 seconds and emulsifying said aqueous phase for 30 seconds. The pre-emulsion thus prepared was then
- homogenized twice at 85°C in a colloid mill with a gap setting of
- 30 1 μm and immediately cooled to 25°C by means of ice, so that a finely divided dispersion of the components of the hydrophobic phase in water was obtained (mean particle diameter 2.6 μm).

35

40

45

TABLE 1

Table 1

| Example | Pressure during the homogenization [bar] | Particle size of the O/W dispersions [μm] | Viscosity of the O/W dispersions [mPas] ²⁾ | Shelf life of the O/W dispersions at 30°C/+5°C in the course of one month | Minimum air content [% by volume] | Long-term effect (5 min) [% by volume] | Tendency to cream according to centrifuge test, 5000 rpm [mm] |
|---------------------|--|--|---|---|-----------------------------------|--|---|
| 1a) | 10 | 3.0 | 100 | homogeneous | 0.24 | 0.17 | 8 |
| 1b) | 20 | 3.0 | 88 | " | 0.24 | 0.18 | 8 |
| 1c) | 40 | 2.1 | 70 | " | 0.23 | 0.13 | 11 |
| 2 | | 2.9 | 20 | " | 0.26 | 0.22 | 5 |
| 3 | | 2.2 | 240 | " | 0.25 | 0.18 | |
| 4 | | 2.2 | 250 | " | 0.22 | 0.13 | |
| 5 | | 4.1 | 65 611) | " | 0.27 | 0.14 | |
| 6a) | 20 | 8.0 | 97 | slight separation into two serial phases | 0.26 | 0.09 | |
| 6b) | 40 | 8.7 | 160 | " | 0.25 | 0.09 | |
| 7) | | 2.6 | 130 | homogeneous | 0.25 | 0.18 | |
| Comparative example | | 4.7 | 530 | creamed | 0.29 | 0.32 | 15 |

1) after addition of 0.7 part of a bisulfonated dodecylidiphenyl oxide

2) measured using a Brookfield viscometer at 20°C and 100 rpm

Example 8

An oil-in-water dispersion in which the oil phase comprised 23.8%
 5 by weight of the dispersion and had a mean particle size of from
 0.2 to 30 μm was prepared with the aid of a Sonotrode (ultrasonic
 probe of the UP 400s type from Dr. Hielscher GmbH).

The oil phase consists of the following components:

10

(a) 3.15 parts of thiaalkanol B

(b) 0.22 part of a polyglyceryl ester which is obtainable by
 complete esterification of a polyglycerol mixture comprising
 15 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol
 and 10% of polyglycerols having a higher degree of
 condensation with behenic acid.

The water phase consisted of:

20

10.6 parts of a 0.4% strength solution of a high molecular weight
 anionic polyacrylamide (molar mass > 1 million) and 0.15 part of
 a 45% strength aqueous solution of the sodium salt of an acrylic
 acid homopolymer having an average molar mass of 2500.

25

Components (a) and (b) were first heated to 90°C and then
 emulsified in the aqueous phase at 95°C with high shearing with
 the Sonotrode for 1 minute and at a power of 20% and immediately
 cooled in an ice bath to room temperature. The properties of the
 30 dispersion thus obtainable are shown in Table 2.

Example 9

An oil-in-water dispersion in which the oil phase comprised 23.8%
 35 of the dispersion was prepared with the aid of an Ultraturrax
 (colloid mill) and a high-pressure homogenizer from
 APV Gaulin GmbH.

The oil phase consisted of the following components:

40

(a) 644 parts of thiaalkanol B

(b) 56 parts of a polyglyceryl ester which is obtainable by
 complete esterification of a polyglycerol mixture comprising
 45 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol

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and 10% of polyglycerols having higher degrees of condensation with behenic acid, and

(c) 254.8 parts of glyceryl triesters of C₁₆-C₁₈-fatty acids.

5

The water phase consisted of:

2454 parts of water, 77.7 parts of a 45% strength aqueous solution of the sodium salt of an acrylic acid homopolymer having
10 an average molar mass of 2500 and 8.75 parts of a high molecular weight anionic polyacrylamide (molar mass > 1 million)

Components (a) to (c) were first heated to 90°C and then emulsified in the aqueous phase at 95°C with high shearing by an
15 Ultraturrax for 2 minutes. This emulsion was then further emulsified at 20, 40 and 60 bar by means of a high-pressure homogenizer from APV Gaulin GmbH and cooled with an ice bath to room temperature immediately after the emulsification. The properties of the dispersions thus obtainable are shown in:
20 Table 2.

Example 10

An oil-in-water dispersion in which the oil phase comprised 23.8%
25 by weight of the dispersion and had a mean particle size of from 0.6 to 8 µm was prepared with the aid of an ultrasonic probe of the UP 400s type from Dr. Hielscher GmbH.

The oil phase consisted of the following components:

30

(a) 3.15 parts of thiaalkanol B

(b) 0.22 part of a polyglyceryl ester which is obtainable by 100% esterification of a polyglycerol mixture comprising 27% of
35 diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with behenic acid.

The water phase consisted of:

40

10.6 parts of a 0.4% strength solution of a high molecular weight anionic polyacrylamide (molar mass > 1 million) and 0.15 part of a 35% strength aqueous solution of an acrylic acid homopolymer having an average molar mass of 100,000. Components (a) and (b)
45 were first heated to 90°C and then emulsified in the aqueous phase at 95°C with high shearing with the Sonotrode for 1 minute and at a power of 20% and immediately cooled in an ice bath to room

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temperature. The properties of the dispersion thus obtainable are shown in Table 2.

Example 11

5

Oil-in-water dispersions in which the oil phase comprise 23.8% by weight of the dispersion were prepared with the aid of an ultrasonic probe of the UP 400s type from Dr. Hielscher GmbH.

10 The oil phase consists of the following components:

(a) 3.15 parts of thiaalkanol B

15 (b) 0.22 part of a polyglyceryl ester which is obtainable by complete esterification of a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having a higher degree of condensation with behenic acid.

20 The water phase consisted of:

10.6 parts of a 0.4% strength solution of a high molecular weight anionic polyacrylamide (molar mass > 1 million),

25 0.03 part of a 45% strength aqueous solution of the sodium salt of an acrylic acid homopolymer having an average molar mass of 2500, and

0.12 part of a 35% strength aqueous solution of an acrylic acid

30 homopolymer having an average molar mass of 100,000.

Components (a) and (b) were first heated to 90°C and then emulsified in the aqueous phase at 95°C with high shearing with the Sonotrode for ½, 1, 1½ and 2 minutes and at a power of 20%

35 and immediately cooled in an ice bath to room temperature. The properties of the dispersion thus obtainable are shown in Table 2.

Example 12

40

An oil-in-water dispersion in which the oil phase comprised 23.8% by weight of the dispersion and had an average particle size of from 0.4 to 15 µm was prepared with the aid of an ultrasonic probe of the UP 400 s type from Dr. Hielscher GmbH.

45

The oil phase consisted of the following components:

(b) 0.22 part of a polyglyceryl ester which was prepared by complete esterification of a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having higher degrees of condensation with behenic acid.

10

15

Example 13

The oil phase consisted of the following components:

30

(b) 0.22 part of a polyglyceryl ester which was prepared by complete esterification of a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having higher degrees of condensation with behenic acid.

40

45

Components (a) and (b) were first heated to 90°C and then emulsified in the aqueous phase at 95°C with high shearing with the Sonotrode for 1 minute and at a power of 20% and immediately cooled to room temperature in an ice bath. The properties of the dispersion thus obtainable were shown in Table 2.

Example 14

An oil-in-water dispersion in which the oil phase comprised 23.8% by weight of the dispersion and had an average particle size of from 0.4 to 10 μm was prepared with the aid of an ultrasonic probe of the UP 400 s type from Dr. Hielscher GmbH.

The oil phase consisted of the following components:

15

(a) 3,15 parts of thiaalkanol B

(b) 0.22 part of a polyglyceryl ester which is obtainable by complete esterification of a polyglycerol mixture comprising 27% of diglycerol, 44% of triglycerol, 19% of tetraglycerol and 10% of polyglycerols having higher degrees of condensation with behenic acid.

25

The water phase consisted of:

10.6 parts of a 0.4% strength solution of a high molecular weight anionic polyacrylamide (molar mass > 1 million),

0.15 part of a 35% strength aqueous solution of an acrylic acid homopolymer having an average molar mass of 100,000 and

0.75 part of a polyethylene glycol having a molar mass of 9000.

Components (a) and (b) were first heated to 90°C and then emulsified in the aqueous phase at 95°C with high shearing with the Sonotrode for 1 minute and at a power of 20% and immediately cooled to room temperature in an ice bath. The physical properties of the dispersion thus prepared are shown in Table 2.

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Table 2

| Example | Duration in min/intensity in % or pressure in bar during homogenization | Particle size distribution in μm | Stability at room temperature within one month | Minimum air content in [% by volume] at 50°C |
|---------|--|--|--|--|
| 1 | 1/20 | 0.2-30 | homogeneous | 0.26 |
| 2 a | 20 bar | | homogeneous | 0.39 |
| 2 b | 40 bar | | homogeneous | 0.27 |
| 2 c | 60 bar | | homogeneous | 0.24 |
| 3 | 1/20 | 0.6-8 | homogeneous | 0.24 |
| 4 a | 0.5/20 | 0.4-30 | homogeneous | |
| 4 b | 1/20 | 0.4-10 | homogeneous | |
| 4 c | 1.5/20 | 0.04-0.5 0.5-8 bimodal | homogeneous | |
| 4 d | 2/20 | 0.06-8 | homogeneous | |
| 5 | 1/20 | 0.4-15 | homogeneous | 0.29 |
| 6 | 1/20 | 0.6-10 | homogeneous | 0.27 |
| 7 | 1.5/20 | 0.4-10 | homogeneous | 0.25 |

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Table 2 (continued)

| Example | Long-term effect (5 min) in [% by volume] at 50°C | Antifoam activity in the foam channel in cm ² at 50°C | Emulsifying apparatus |
|---------|---|--|-----------------------|
| 1 | 0.26 | 210 | ultrasonic |
| 2 a | 0.25 | 220 | homogenizer |
| 2 b | 0.29 | 230 | homogenizer |
| 2 c | 0.37 | 230 | homogenizer |
| 3 | 0.20 | 250 | ultrasonic |
| 4 a | | 240 | ultrasonic |
| 4 b | | 230 | ultrasonic |
| 4 c | | 230 | ultrasonic |
| 4 d | | 230 | ultrasonic |
| 5 | 0.26 | 210 | ultrasonic |
| 6 | 0.21 | 220 | ultrasonic |
| 7 | 0.13 | 170 | ultrasonic |